RESTORATION OF THE WORKING BODY OF THE JOHN DEERE 512 DISK RIPPER WITH MULTI-LAYER FRONT SURFACING

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Abstract. Modern technologies of soil cultivation during cultivation of agricultural crops are aimed at reducing mechanical action due to a justified reduction in the number of technological operations, as well as combining several operations on the technological platform of one machine-tractor unit, performed in one pass. One of the ways to reduce the impact on the soil is to exclude formation turnover during continuous tillage (plowing). For this, deep rippers of various designs are used. The common element for them are the working bodies - metal-intensive racks with cutting and crushing surfaces. Due to the difficult working conditions, including a large mass of the unit, high dynamic loads and intense abrasive wear, they determine the failure-free, long-eternity and maintainability of the structure. An analysis of the wear of the tip under operating conditions showed that the limiting state occurs when an average loss of 8.5 % of the weight of the tip by weight wear occurs. The results of micrometeringshowed that the limiting state was linearly changed by the “toe-heel” parameter at an average of 9.7 %, and by the “toe-anterior hole” parameter, an average of 16 % of the new value. Therefore, the obvious fact is the presence of 84-90 % of the unused residual resource. In the laboratory of restoration of worn parts of the Belgorod State Agrarian University, the technology of frontal cladding with annealing rollers using heat-treated elements was developed to restore the tips of the working bodies of the 512 Disk Ripper. The incomplete use of the resource of the tip of the deep ripper was established when replacing it according to the manufacturer’s recommendations. The presence of the residual resource of the part by mass allows to repeatedly restore its operational state. The proposed technology for restoring the tip is 47 % cheaper than purchasing new ones. Moreover, their resource is increased by 50 %.

Key words: anchor, working body, wear, residual resource, restoration, surfacing, durability.

Introduction

Modern technologies of soil cultivation during the cultivation of agricultural crops are aimed at reducing mechanical action due to a justified reduction in the number of technological operations, as well as combining several operations on the technological platform of one machine-tractor unit, performed in one pass [1-3].

One of the ways to reduce the impact on the soil is to exclude formation turnover during continuous tillage (plowing). For this, deep rippers of various designs are used. The common element for them are the working bodies - metal-intensive racks with cutting and crushing surfaces. Due to the difficult working conditions, including a large mass of the unit, high dynamic loads and intense abrasive wear, they determine the failure-free, long-eternity and maintainability of the structure [4-6].

If a failure occurs, it is necessary to restore the working state of the part, node, or unit. The existing system is reduced to dealer supply of spare parts and consumables. In this case, the operating costs for maintaining the equipment in working condition increase sharply. The results of experimental restoration of parts of foreign equipment showed that the use of various technologies can reduce the cost of spare parts. In addition, their repeated use makes it possible to solve economic and environmental problems of mechanical engineering in many ways [7].

There are several methods for volumetric wear compensation. Filling with liquid metal does not provide high-quality adhesion to the base, does not guarantee the necessary carbon content in the alloy, and requires special metallurgical equipment. Surfacing with an electric arc and flame leads to the appearance of shrinkage thermal cracks during cooling and a decrease in adhesion to the base.

Materials and methods

The 512 Disk Ripper (Fig. 1) is characterized by a two-element design of the working body, which includes a stand providing load-bearing capacity, and a removable tip designed for loosening the soil to a depth of 60 cm. The tip directly contacts the soil abrasive at high contact pressure and, in this regard, is a “weak” structural element with a resource significantly less than the life of the rack, the failure of which occurs due to fatigue or catastrophic failure.

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The Ripper 512 design provides increased reliability by providing a high level of maintainability. This is manifested in the replacement of a quick-wear element—the anchor (tip), and not the entire rack. It is supplied by the dealer as spare part with high added value. However, their resource is not increased, and manufacturers do not provide measures to improve wear resistance. The resource is provided by the structural material—high-strength cast iron, from which the tip is made by casting. A number of studies have been conducted to assess the possibility of carrying out renovation activities.

In the laboratory of restoration of worn parts of the Belgorod State Agrarian University, the technology of frontal cladding with annealing rollers using heat-treated elements was developed to restore the tips of the working bodies of the 512 Disk Ripper.

It is proposed to perform electric arc welding by successively applying layers of molten metal on top of each other with the inclusion of heat-strengthened elements with high carbon content. This reduces thermal cracking due to annealing at high carbon content.

With this technology, the part is restored to its nominal parameters. Surfacing was carried out in a protective (carbon dioxide) gas environment with a semi-automatic welding machine using a self-fluxing wire of H10X10G10T diameter 1.2 mm. As a heat-strengthened element, a strip of spring steel after heat treatment with a hardness of HRC 50.55 units is taken. During the surfacing process, a special method of “annealing rollers” eliminates the possibility of “bleaching” cast iron and the formation of shrink cracks. At the end of formation of the missing part of the anchor, the surface in contact with the abrasive was deposited with a wear-resistant material using T590 electrodes.

Operational parameters of the technological process were determined experimentally. Current strength was measured by the scale of the apparatus for surfacing. Weight parameters were determined using weights (accuracy 5 g). Linear parameters were determined using a caliper (accuracy 0.1 mm, class 1). Temperature was measured using a C-550.1 pyrometer with a range of 400-1600.

The durability test of the samples was carried out on a SMT-1 friction machine by a relative comparison of the two samples. The rollers were made of anchor material and with a deposited layer. Rotational speed is 500 min\(^{-1}\), the load is 1000 N, and duration is 60 min. Medium is an aqueous suspension of silica sand.

To process the experimental data, we used methods of statistical analysis of reliability indicators and a standard package of Excel application programs.

**Results and discussion**

Analysis of the wear of the tip under operating conditions showed (Fig. 2) that the limit state occurs, when an average of 0.9 kg or 8.5 % of the tip weight is lost due to weight wear. The results of micrometering showed that the linear change in the “toe-heal” parameter reached the limit on average with a decrease in size by 34.2 mm or 9.7 %, and the “toe-front hole” parameter reached the limit on average with wear of 65.8 mm or 16 % of the values of the new anchor. Therefore, the obvious fact is the presence of 84-90 % of the unused residual resource of the anchor. The average square deviation was no more than 10 g for weight wear and 1-3 mm for linear wear.
The main technological parameter for surfacing is the current strength. Experimental studies have shown that in the range of 90-120 A, recommended by the manufacturer of the surfacing material, a current of 110 A is optimal. In this case, the part does not overheat and the spray loss (lack of penetration) is minimal (Table 1). The choice was made according to the heating temperature and the output of the surfacing material (mass of wire before surfacing / mass of metal deposited on the part * 100 % = loss of material in %).

**Table 1**

<table>
<thead>
<tr>
<th>Amperage, A</th>
<th>Temperature of the heating part, ºC</th>
<th>Loss of material, %</th>
</tr>
</thead>
<tbody>
<tr>
<td>90</td>
<td>852</td>
<td>8</td>
</tr>
<tr>
<td>95</td>
<td>910</td>
<td>6</td>
</tr>
<tr>
<td>100</td>
<td>960</td>
<td>3</td>
</tr>
<tr>
<td>105</td>
<td>1010</td>
<td>2</td>
</tr>
<tr>
<td>110</td>
<td>1012</td>
<td>1</td>
</tr>
<tr>
<td>115</td>
<td>1108</td>
<td>4</td>
</tr>
<tr>
<td>120</td>
<td>1218</td>
<td>6</td>
</tr>
</tbody>
</table>

Studies of changes in the surface resistance against abrasive wear showed (Fig. 3) that surface ligation during frontal surfacing using annealing rollers with a heat-strengthened (high-carbon) element increases the wear resistance compared to the anchor material by 2.4 times, and when applying an additional wear-resistant electrode material T590 - by 5.6 times.

**Fig. 3. Potential for increased durability when restoring**

The restored anchors in all geometric parameters corresponded to the nominal sizes of the new one (Fig. 4).
After restoration and hardening, the nature of the wear process changes (Fig. 5). The wear rate of the front part is reduced, while ensuring the implementation of the “self-sharpening” effect. This leads to a decrease in the resistivity of the working body.

During the development of the technological process, the possibility of re-restoration of the anchor surface was checked. The difference between the technological process for the second and third surface restoration is the amount of the applied surfacing material. At the third restoration, it is 3-5 % more (Fig.6). It was found that the cutting surface of the anchor after the third restoration wears out 1.15 times slower than the anchor after the second restoration (Fig. 7). This is due to metallurgical processes during repeated surfacing.

However, the feasibility of recovery is lost when weight wear is 28-32 % of the weight of the new anchor. This is due to the wear not of the front surface of cutting and crumbling, but to the loss of
mass of the side surfaces of the anchor and its “wings”. The remains of a previously restored and strengthened surface are seen in Fig. 8. In this case, the loosening process is completely disrupted.

Fig. 8. View of the extremely worn-out anchor that cannot be restored

Operation in real conditions of the Sukmanovka SPK in the Belgorod region showed an increase in the resource from 600 ha to 900 ha at a processing depth of 25.30 cm on loam and sandy loam soils.

Conclusions

So, the incomplete use of the resource of the tip of the deep ripper was established, when replacing it according to the manufacturer’s recommendations. The presence of the residual resource of the part by mass allows to repeatedly restore its operational state. The proposed technology for restoring the tip by front surfacing with annealing rollers with the use of heat-treated elements and subsequent application of a wear-resistant coating T590 restores it to its nominal size and completely resumes its working state. When using the surfacing wire NP-30H10G10T with a diameter of 1.2 mm, the surfacing should be carried out at a current of 110 A. Potentially, the resource can be increased by 2.44-5.50 times. In real operating conditions, its increase is by 1.5 times. The use of this recovery method makes anchors at the first restoration 47 % cheaper than new ones. Renovation of handpieces increases their resource by 50-54 %. The third and subsequent renewal of the resource provides a superprofit due to the full depreciation of anchors.

References


